Improved Structure and Long-life Blanket Concepts for Heliotron Reactors

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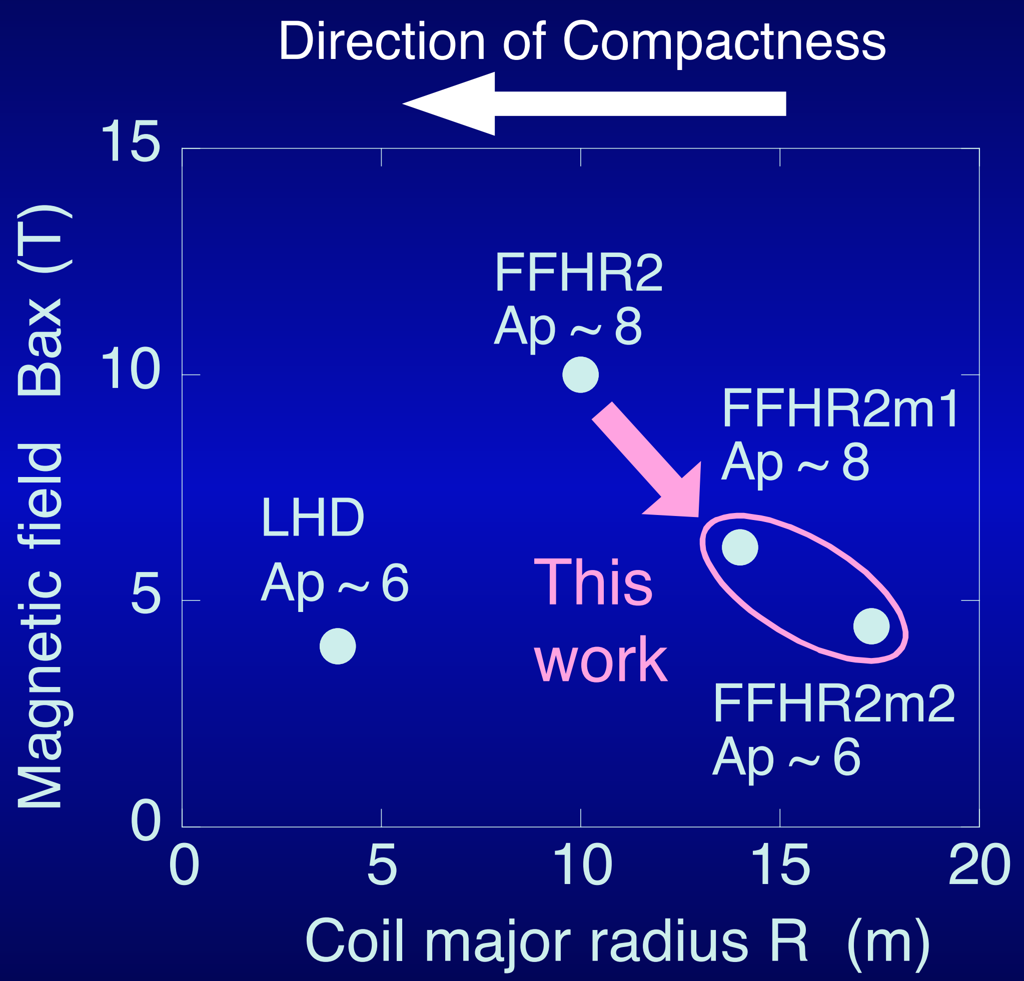
Presentation Outline



1. Introduction of FFHR

2. New design approach
   - The size is increased
   - Why ?

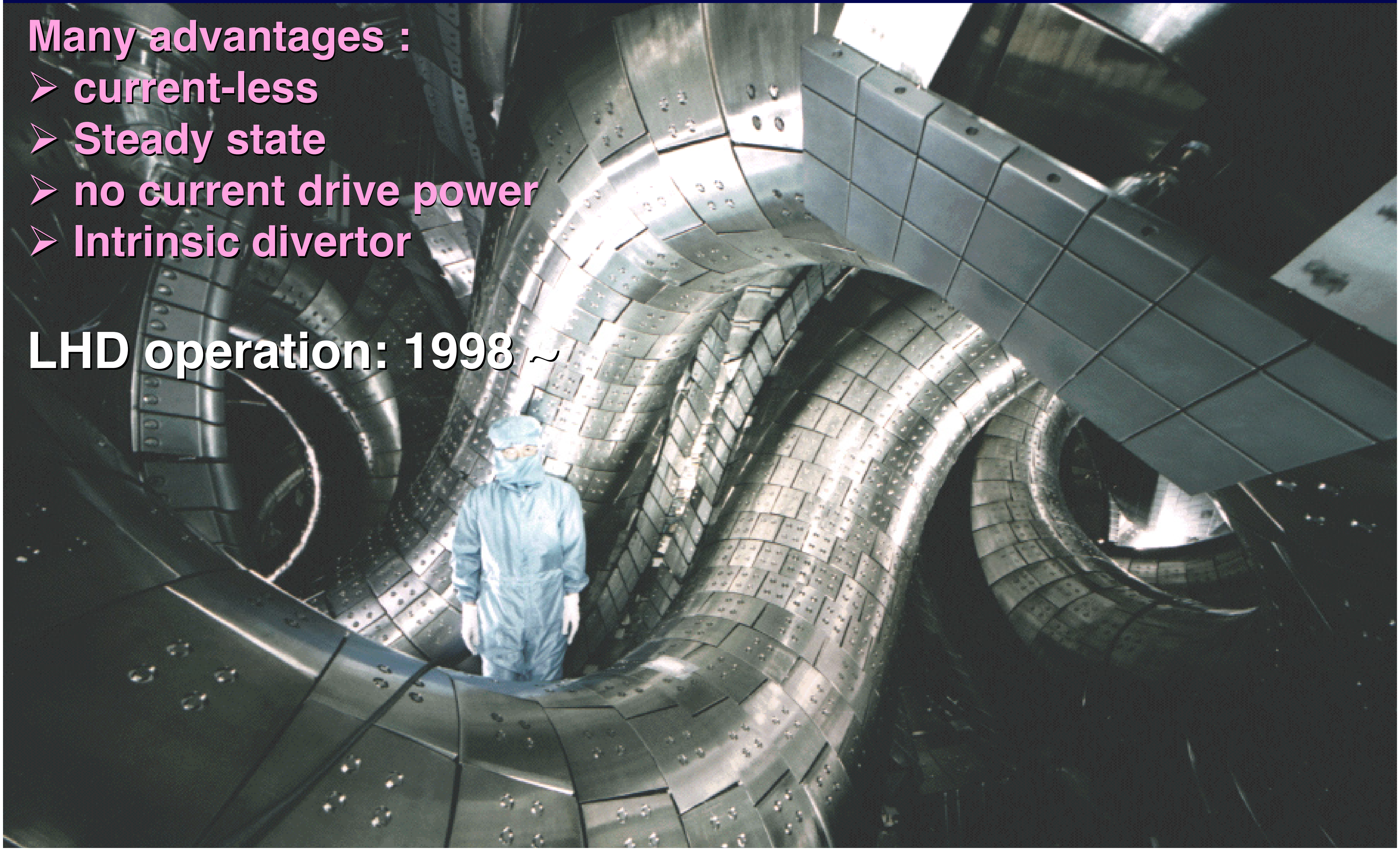
3. Conclusions

LHD-type D-T Reactor FFHR

Many advantages :

- current-less
- Steady state
- no current drive power
- Intrinsic divertor

LHD operation: 1998 ~



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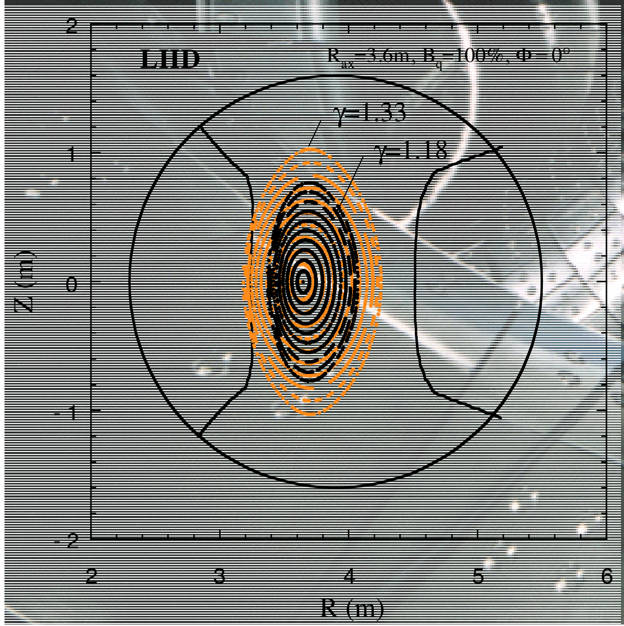


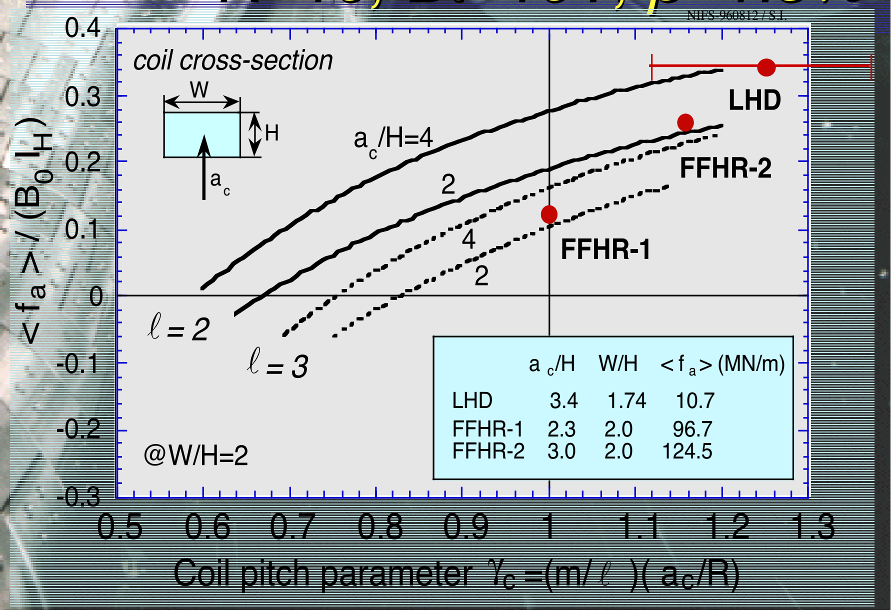
$\gamma = \tan\theta$

Selection of lower $\gamma = \left(\dfrac{m}{l}\dfrac{a_c}{R}\right)$

- To reduce mag. foop force
- To expand blanket space

1993 FFHR-1 (*l=3, m=18*)
R=20, Bt=12T, β=0.7%

1995 FFHR-2 (*l=2, m=10*)
R=10, Bt=10T, β=1.8%



	a_c/H	W/H	$< f_a >$ (MN/m)
LHD	3.4	1.74	10.7
FFHR-1	2.3	2.0	96.7
FFHR-2	3.0	2.0	124.5

However, direction of compact design has engineering issues

- Insufficient tritium breeding ratio (TBR)
- Insufficient nuclear shielding for superconducting (SC) magnets,

Blanket space limitation

- Replacement of blanket due to high neutron wall loading
- Narrowed maintenance ports due to the support structure for high magnetic field

Replacement difficulty

New design approach is proposed to overcome all these issues

- Introducing a long–life & thicker breeder blanket
- Increasing the reactor size with decreasing the magnetic field
- Improving the coils-support structure

$\left.\begin{array}{l}\text{Introducing a long–life \& thicker breeder blanket} \\ \text{Increasing the reactor size with decreasing the magnetic field}\end{array}\right\}$ Blanket space

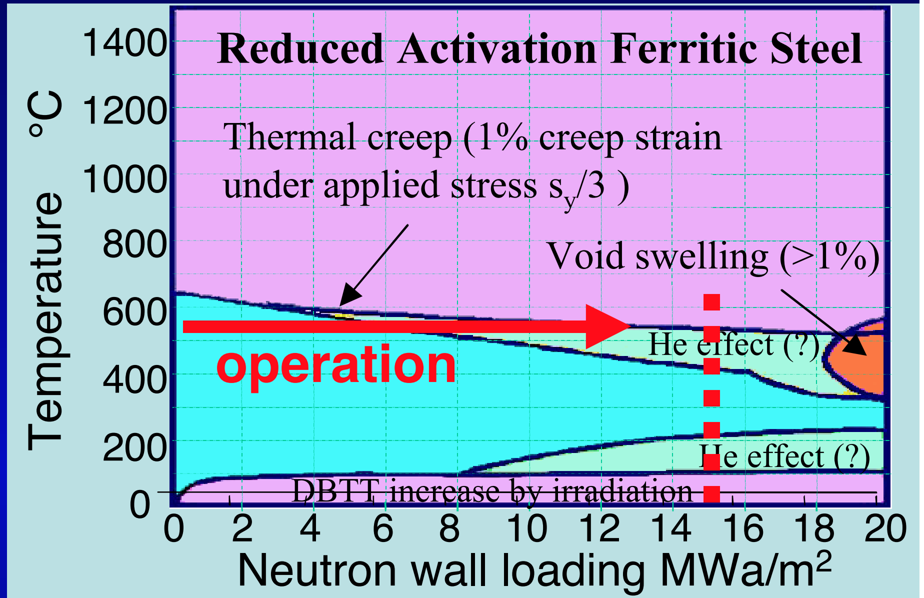
$\left.\begin{array}{l}\text{All three}\end{array}\right\}$ Replacement

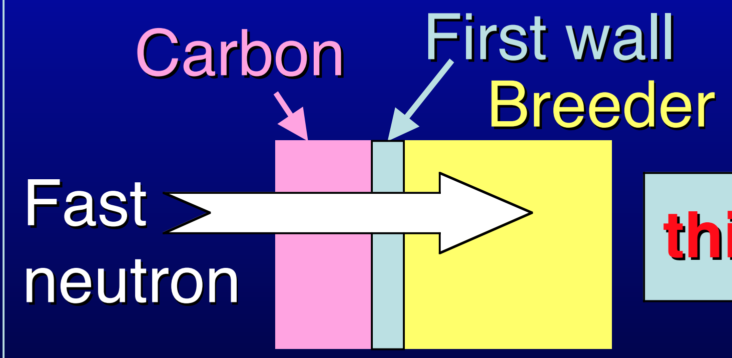
Proposal and Optimization of STB
(Spectral-shifter and Tritium breeder Blanket)

- Lifetime of Flibe/RAFS liquid blanket in FFHR ~ 15MWa/m^2

factor 3

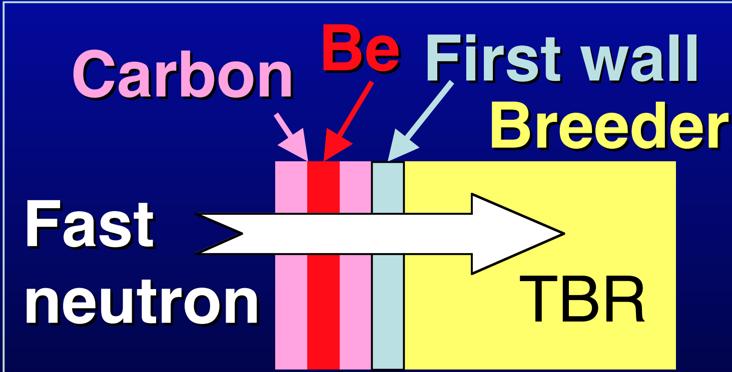
- Neutron wall loading in FFHR2 in 30 years
1.5MW/m^2 x 30y = 45MWa/m^2





ISSEC : by Kulchinski, '75

this work



STB & optimization

Proposal and Optimization of STB (Spectral-shifter and Tritium breeder Blanket)

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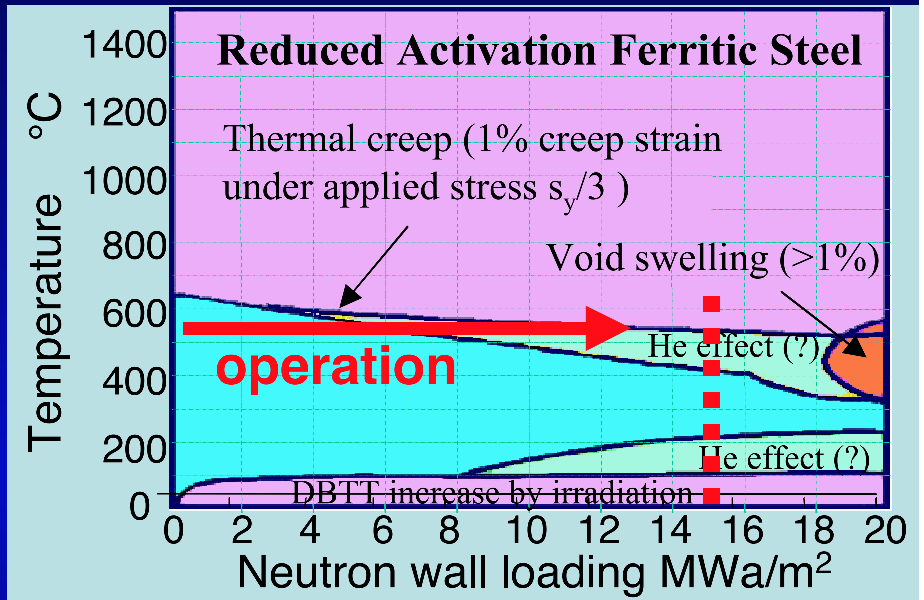
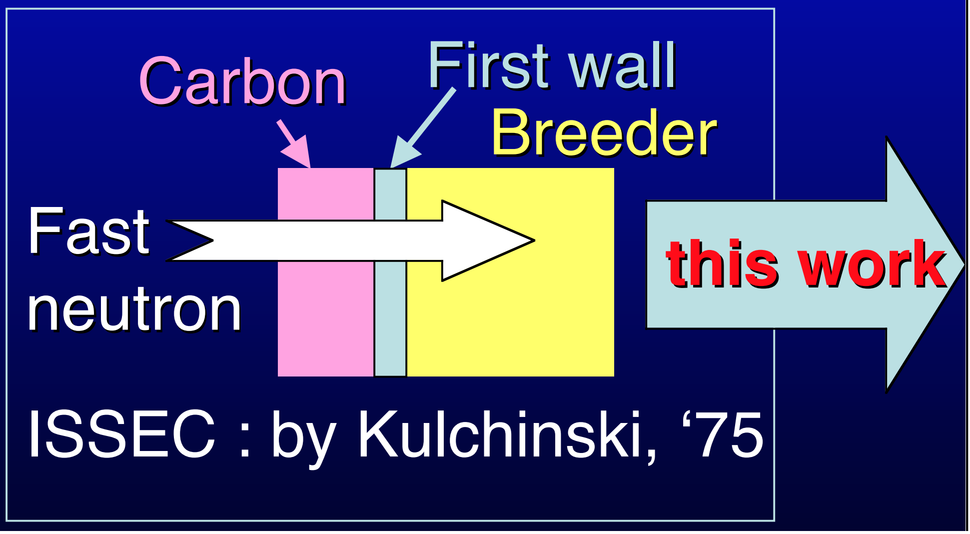
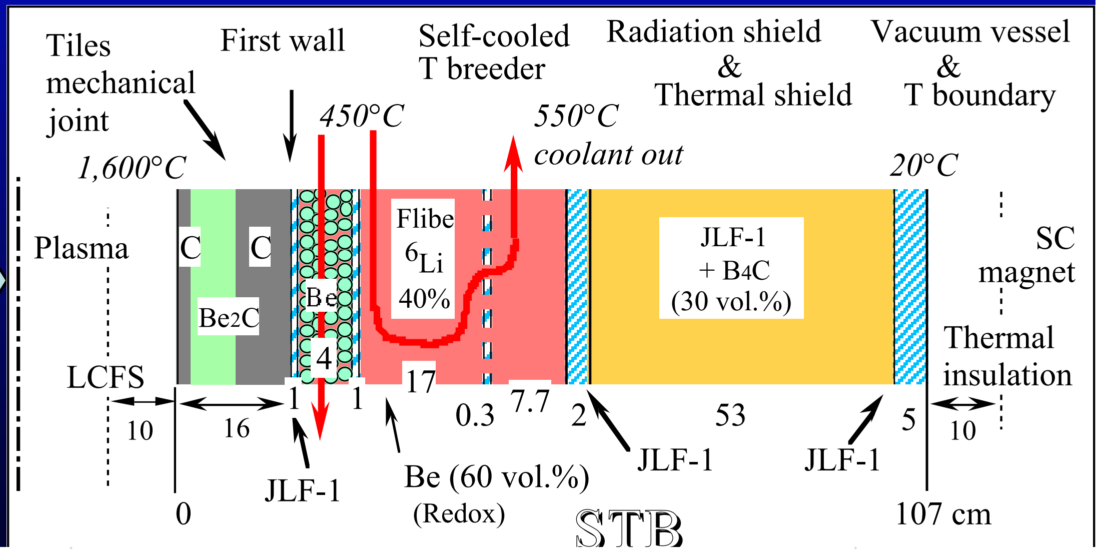
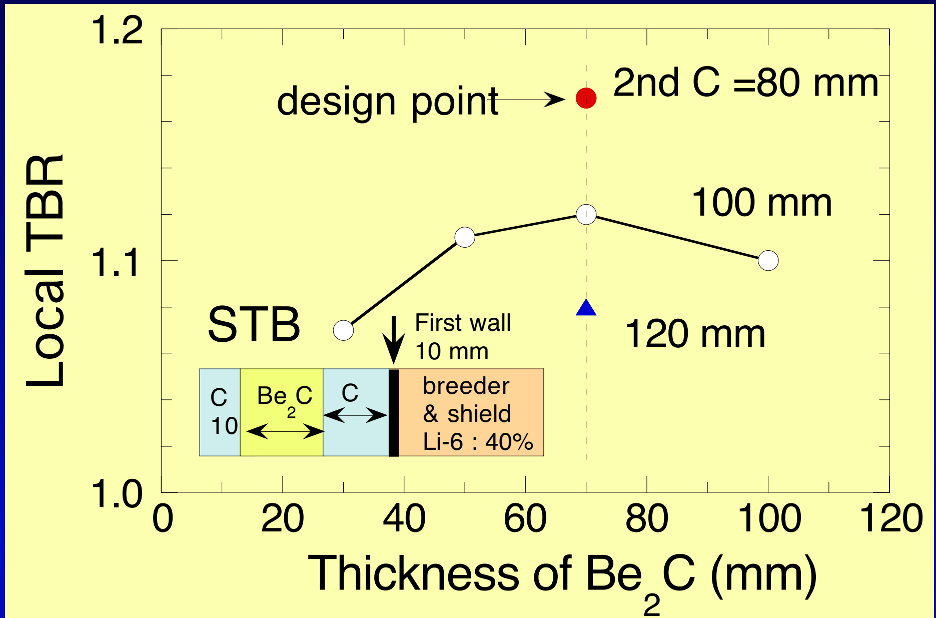
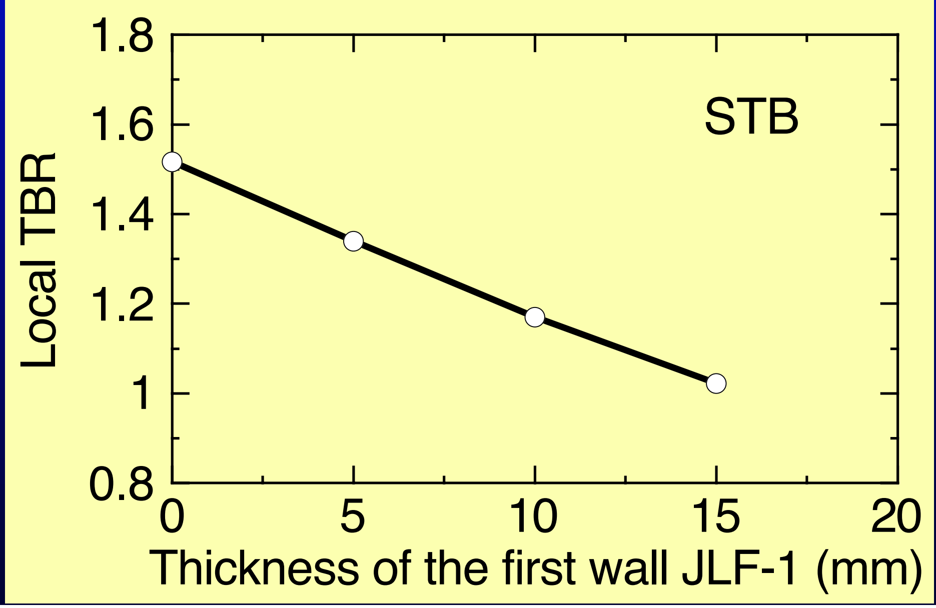




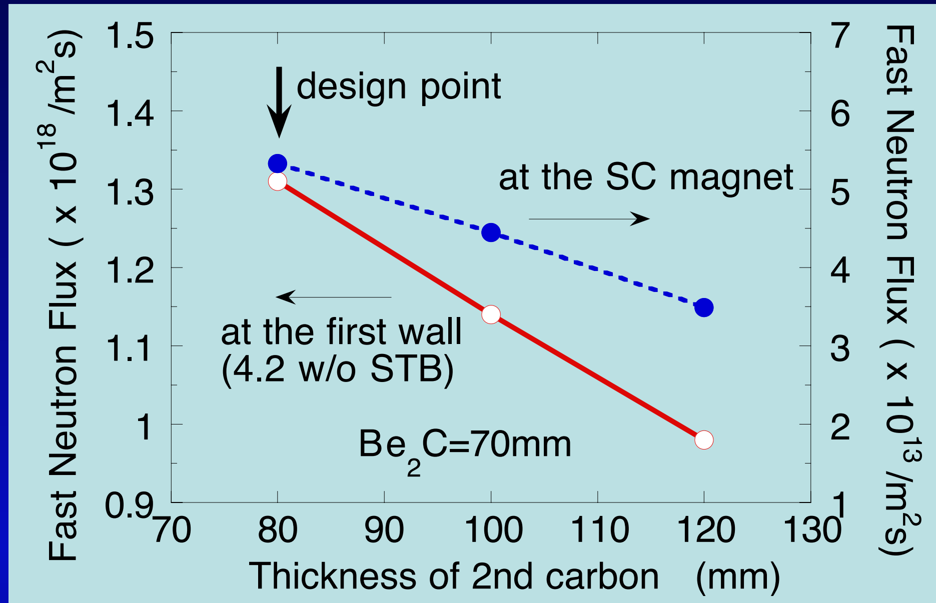


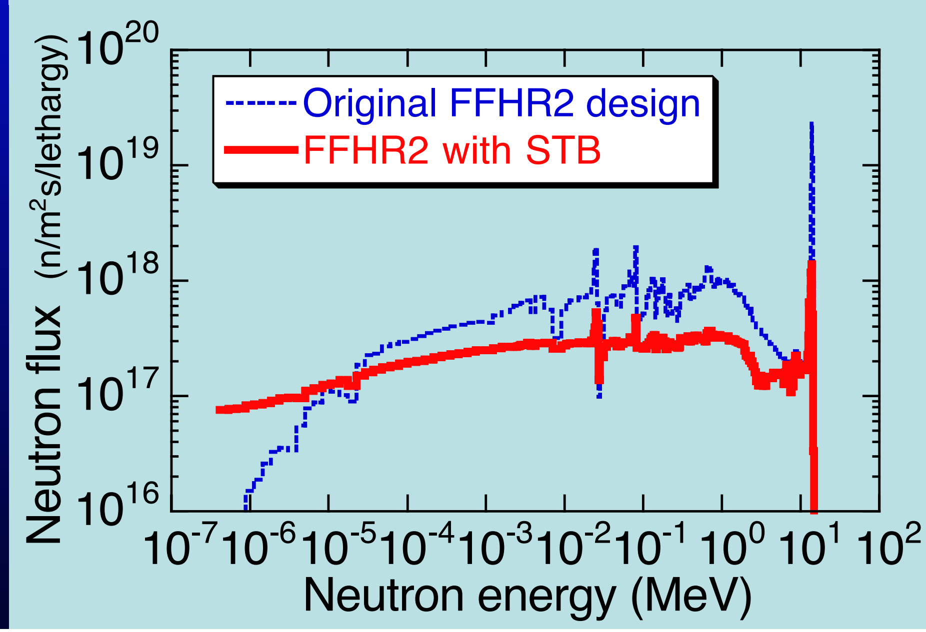
Tritium breeding



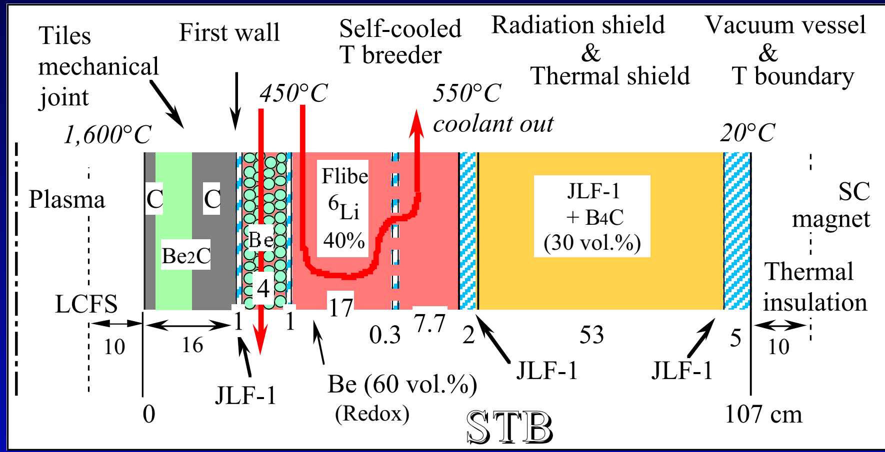


Shielding efficiency





Results and Key R&D Issues



Results :

- ✓ Fast neutron flux at the first wall is factor 3 reduced.
- ✓ Local TBR > 1.2 is possible.
- ✓ Fast neutron fluence to SC is reduced to 5×10^{22} n/m^2 (Tc/Tco>90% in 30y)
- ✓ Surface temperature < 2000°C(~mPa of C) is possible

Key R&D issues :

(1) Impurity shielding in edge plasma

(2) Neutron irradiation effects on tiles at high temperature

(3) Heat transfer enhancement in Flibe flow

Required conditions :

- ➢ Neutron wall loading < 1.5MW/m^2
- ➢ Blanket thickness > 1100 mm

Design parameter

- ➢ λ for C-Be-C tiles > 100W/mK
- ➢ Super-G sheet for tiles joint > 6kW/m^{2}K
- ➢ Heat removal by Flibe > 1MW/m^2

Improved design parameters

Improved input

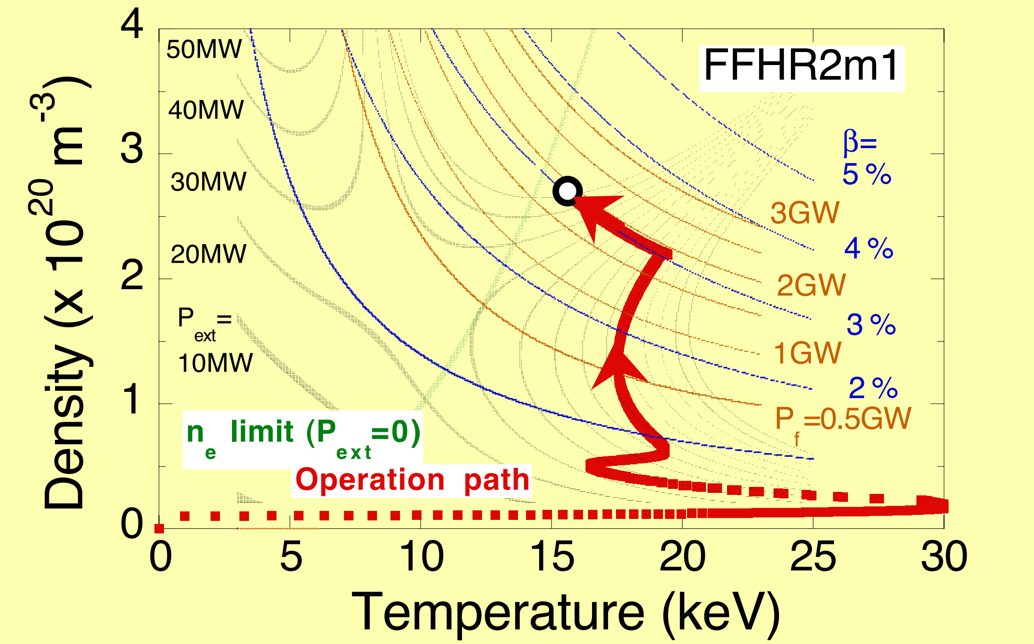
Required Blanket space

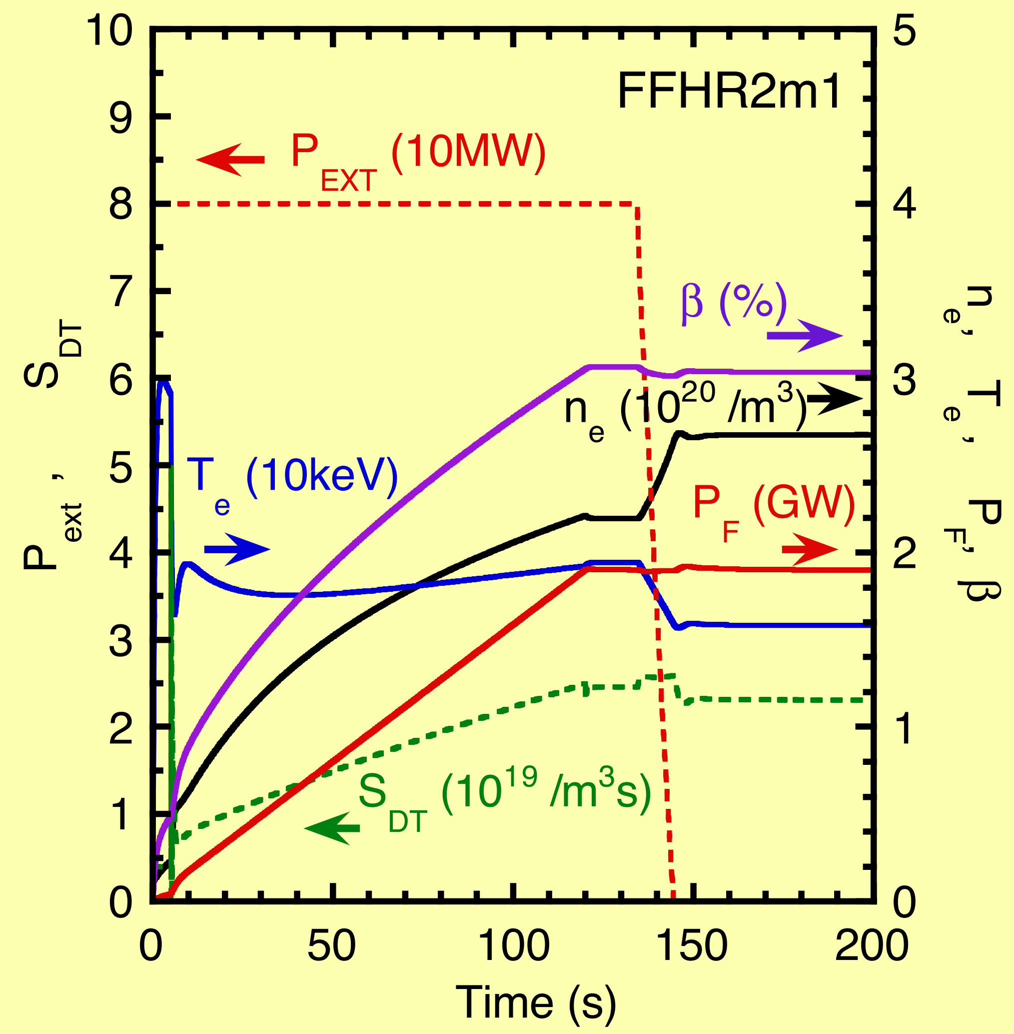
Required Wall loading

$$\tau_{ISS95} = 0.26 P^{-0.59} \bar{n}_e^{\,0.51} B^{0.83} R^{0.65} a^{2.21} \iota_{2/3}^{\,0.4}$$

Design parameters			LHD	FFHR2	FFHR2m1	FFHR2m2
Polarity	l		2	2	2	2
Field periods	m		10	10	10	10
Coil pitch parameter	γ		**1.25**	**1.15**	**1.15**	**1.25**
Coil major Radius	Rc	m	3.9	10	14.0	17.3
Coil minor radius	ac	m	0.98	2.3	3.22	4.33
Plasma major radius	Rp	m	**3.75**	**10**	**14.0**	**16.0**
Plasma radius	ap	m	0.61	1.2	1.73	2.80
Blanket space	Δ	m	0.12	**0.7**	**1.2**	**1.1**
Magnetic field	B0	T	**4**	**10**	**6.18**	**4.43**
Max. field on coils	Bmax	T	9.2	13	13.3	13
Coil current density	j	MA/m2	53	25	26.6	32.8
Weight of support		ton	400	**2880**	**3020**	**3210**
Magnetic energy		GJ	1.64	147	120	142
Fusion power	P_F	GW		**1.77**	**1.9**	**3.0**
Neutron wall load		MW/m2		**2.8**	**1.5**	**1.3**
External heating power	Pext	MW		100	80	100
α heating efficiency	$\eta\alpha$			0.7	0.9	0.9
Density lim.improvement				1	1.5	1.5
H factor of ISS95				**2.53**	**1.92**	**1.68**
Effective ion charge	Zeff			1.32	1.34	1.35
Electron density	ne(0)	10^19 m-3		28.0	26.7	19.0
Temperature	Ti(0)	keV		27	15.8	16.1
$\langle\beta\rangle=2*n*T/(B^2/\mu)$ (parabolic distribution)				**1.8**	**3.0**	**4.1**
COE		Yen/kWh		**21.00**	**14.00**	**9.00**

Self-ignition access in FFHR2m1





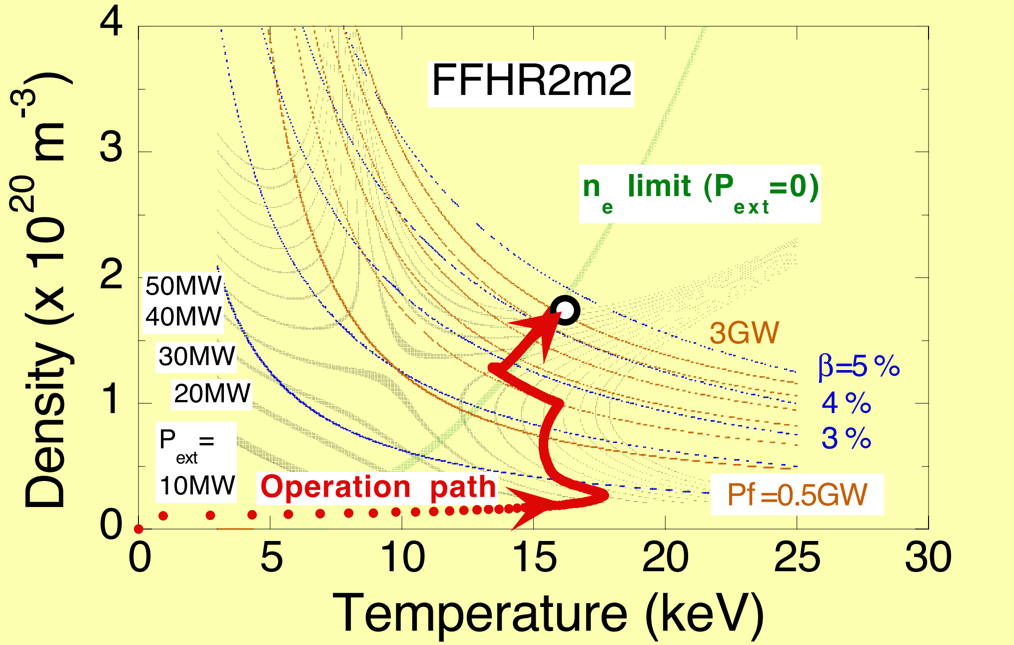
Zero-dimensional analysis

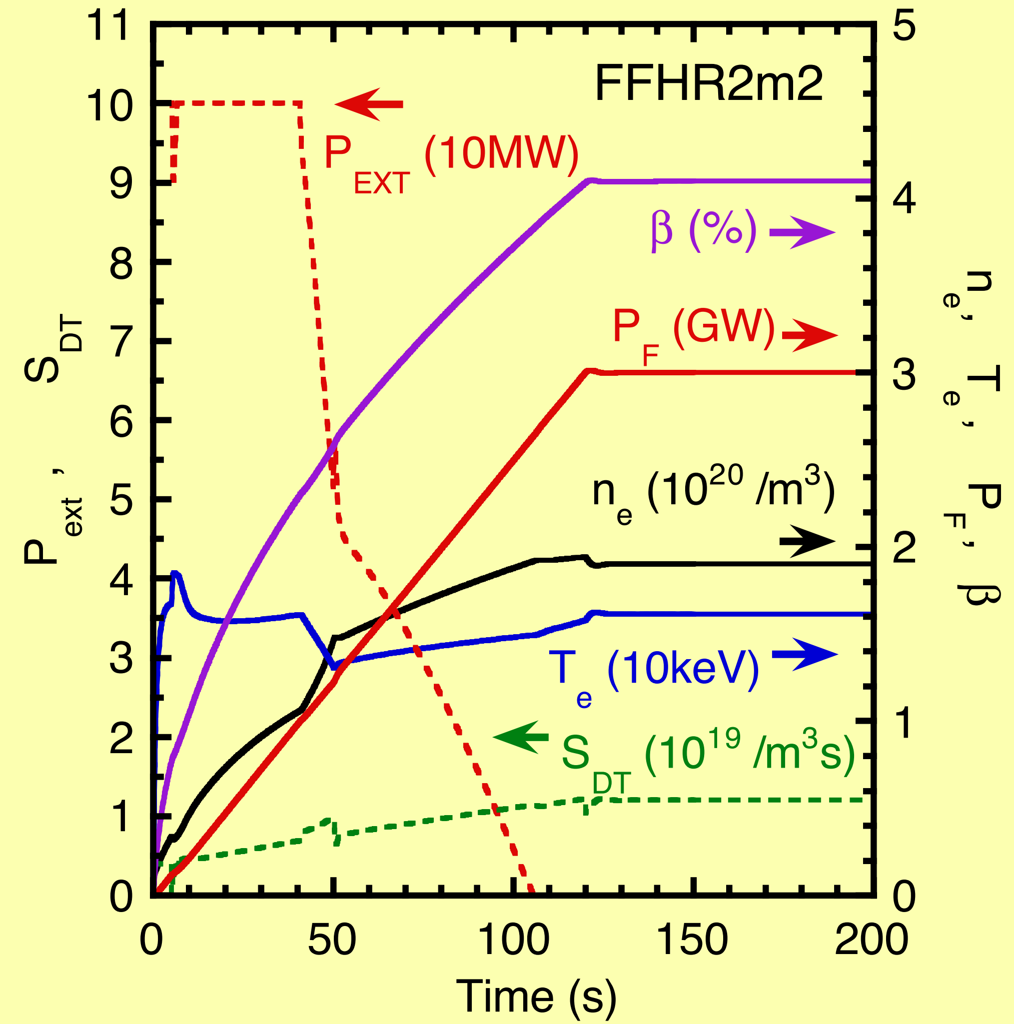
- H_{ISS95} = 1.2 x 1.6
- $\tau^*_\alpha / \tau_E = 3$ (< 7)
- parabolic profiles
- n_e < 1.5 x Sudo limit
- α heating efficiency = 0.9

Already achieved in LHD

O.Mitarai et al., Fusion Eng. Design 70 ('04) 247.

Self-ignition access in FFHR2m2





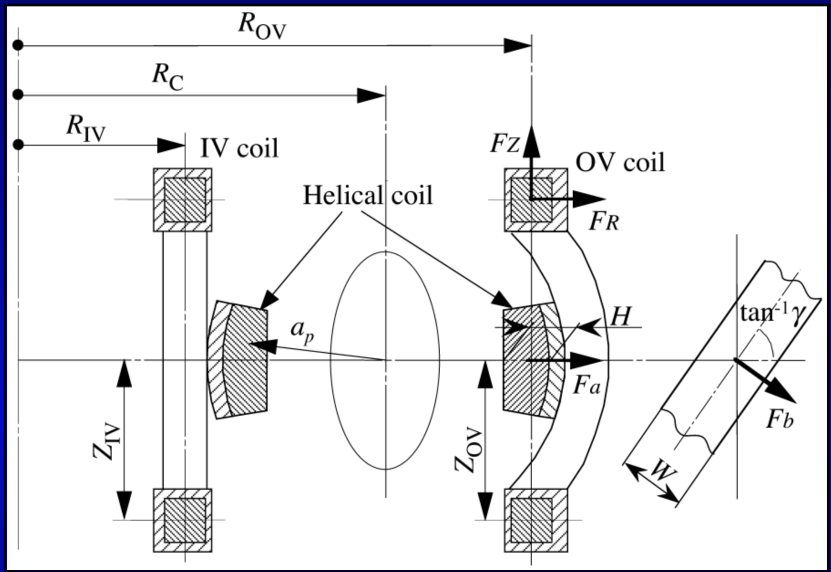
Zero-dimensional analysis

- H_{ISS95} = 1.1 x 1.6
- τ^*_α / τ_E = 3 (< 7)
- parabolic profiles
- n_e< 1.5 x Sudo limit
- α heating efficiency = 0.9

Already achieved in LHD

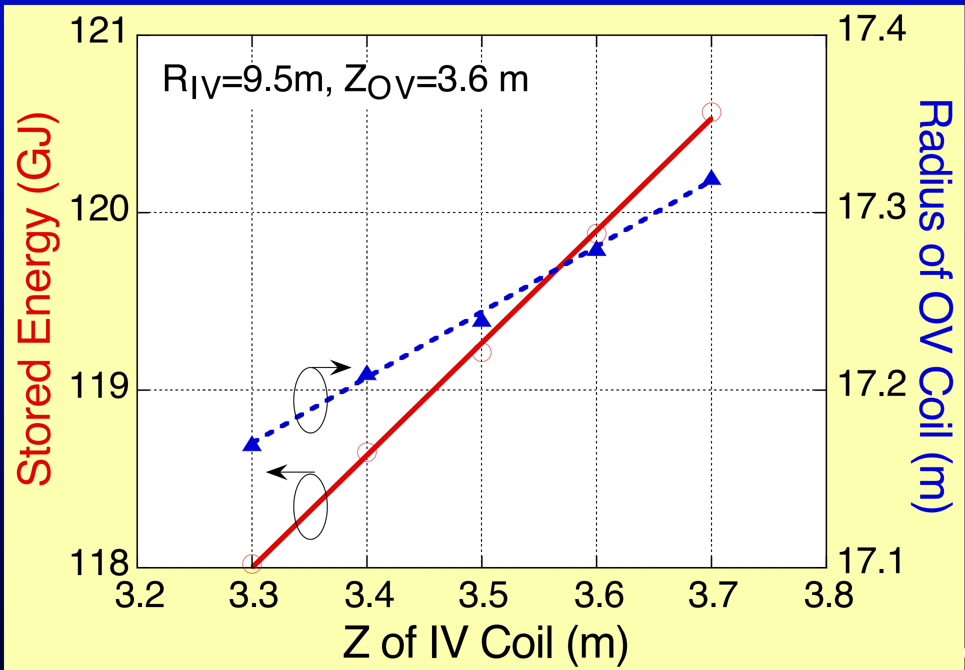
O.Mitarai et al., Fusion Eng. Design 70 ('04) 247.

Improved Design of Coil-supporting Structure (1/2)



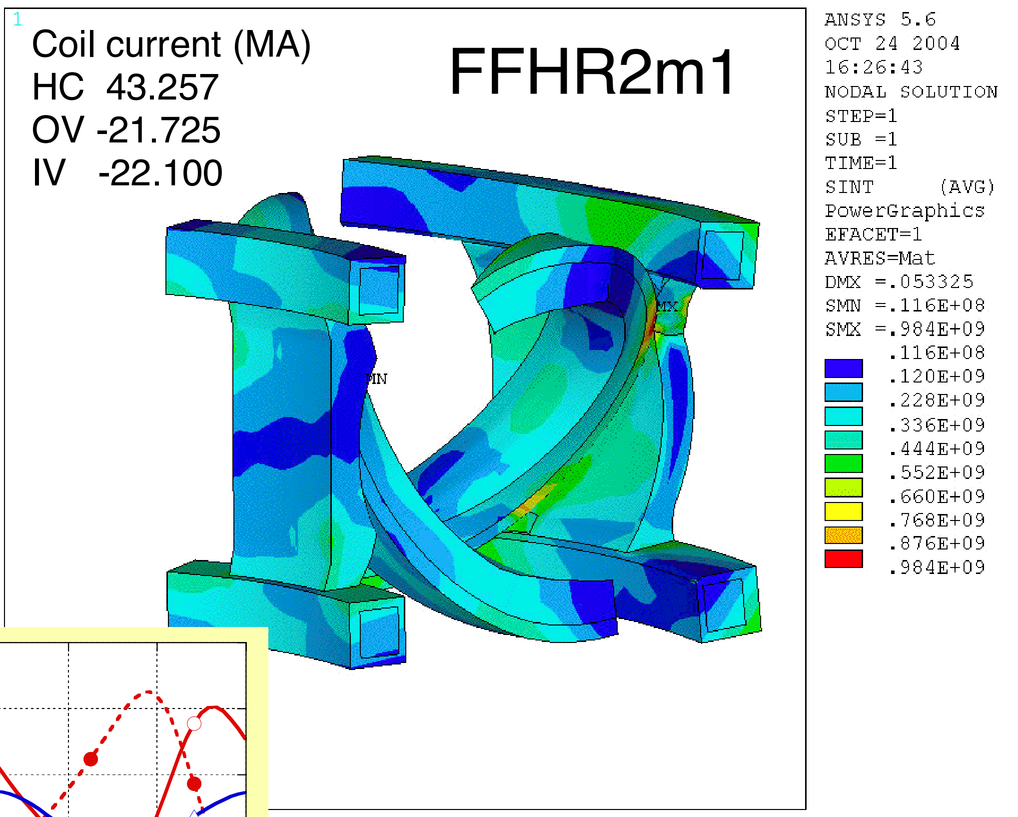
- **Cylindrical supporting structure under reduced magnetic force,** which facilitates expansion of the maintenance ports.
- **Helical coils supported at inner, outer and bottom only.**

- **W/H = 2 & H/a_c determined by**
- **Bmax ~ 13 T for such as Nb_3Sn or Nb_3Al.**
- **Then J=25~35A/mm^2**
- **Poloidal coils layout as for stored magnetic energy and stray field**

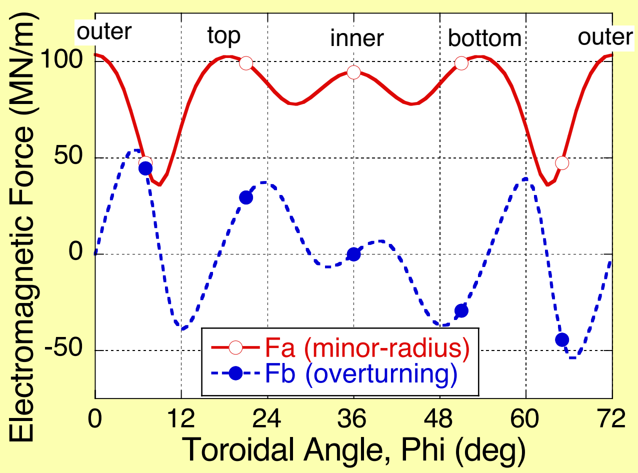


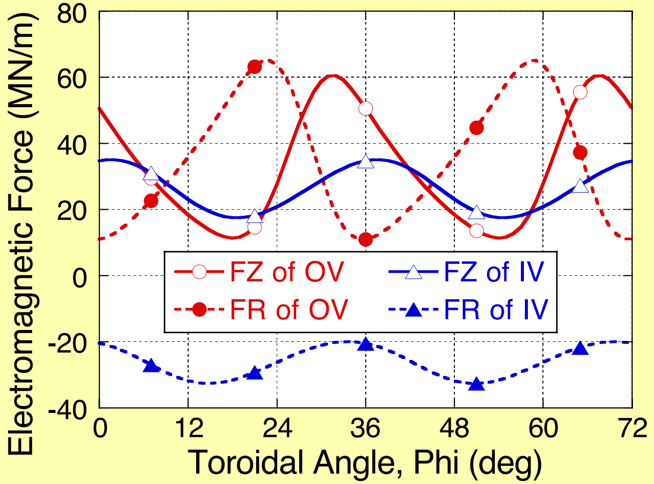
Improved Design of Coil-supporting Structure (2/2)

- The maximum stress can be reduced less than 1000 MPa (<1.5Sm)
- This value is allowable for strengthened stainless steel.



Electromagnetic forces on a helical coil of FFHR2m1.

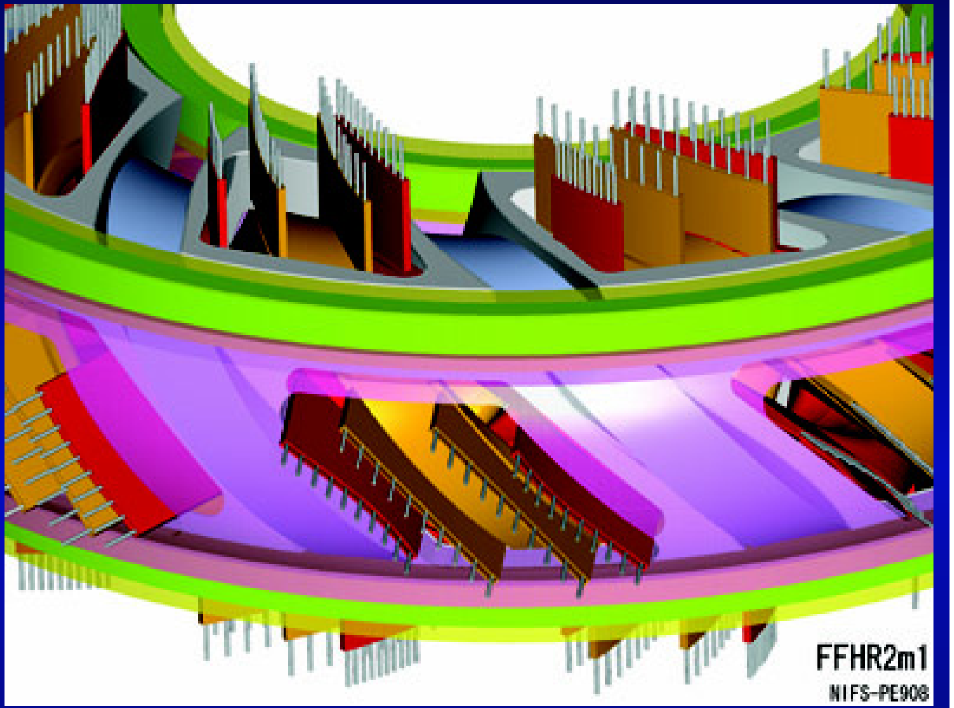


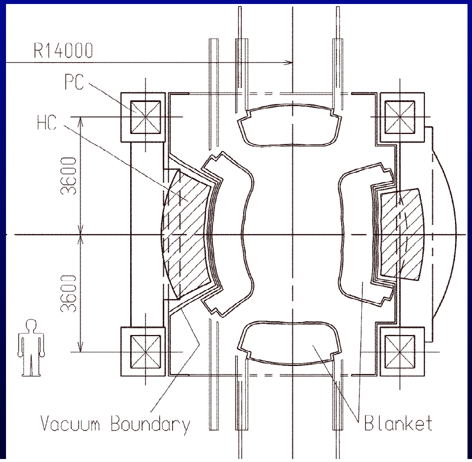


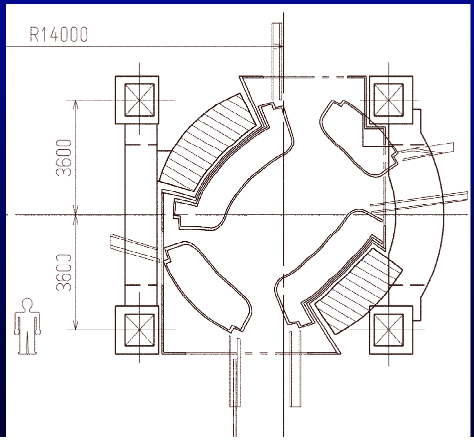
on poloidal coils

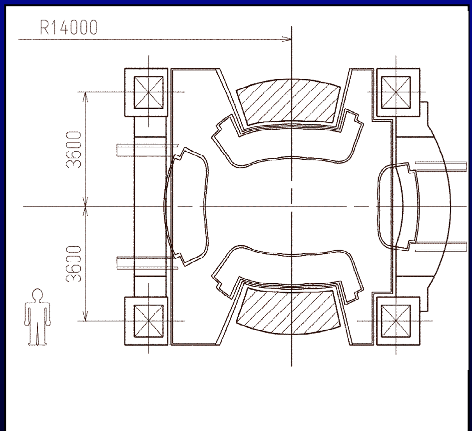
Replacement of In-Vessel Components (1/2)

- **Large size maintenance ports** at top, bottom, outer and inner sides.
- **The vacuum boundary located** just inside of the helical coils and supporting structure.
- **Blanket units supported on the permanent shielding structures,** which are mainly supported at their helical bottom position.





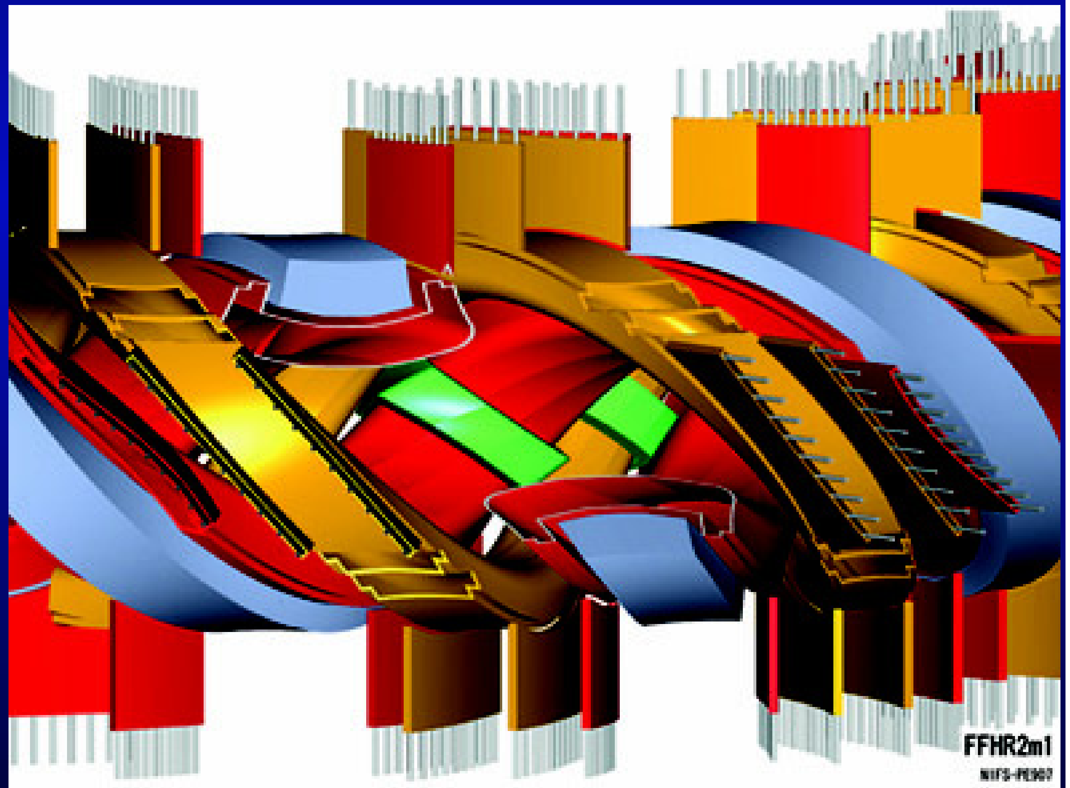




Replacement of In-Vessel Components (2/2)

Proposal of the "Screw coaster" concept to replace STB armor tiles

- **Replacement of bolted tiles** during the planned inspection period.
- **Using the merit of helical structure,** where the normal cross section of blanket is constant.
- **Toroidal effects can be adjusted** with flexible actuators.

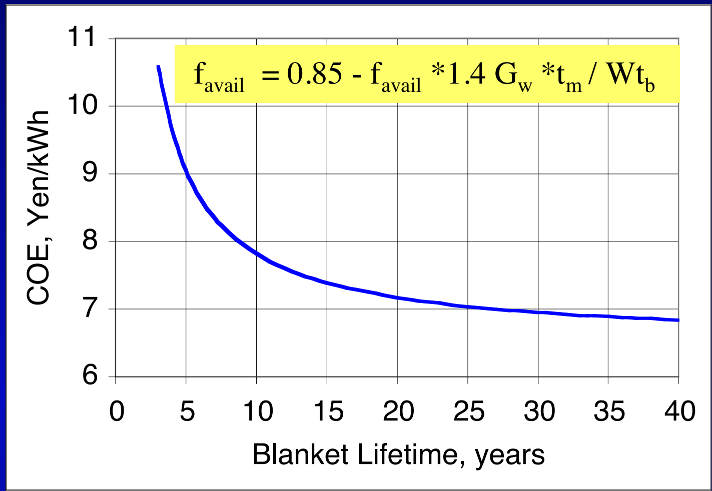


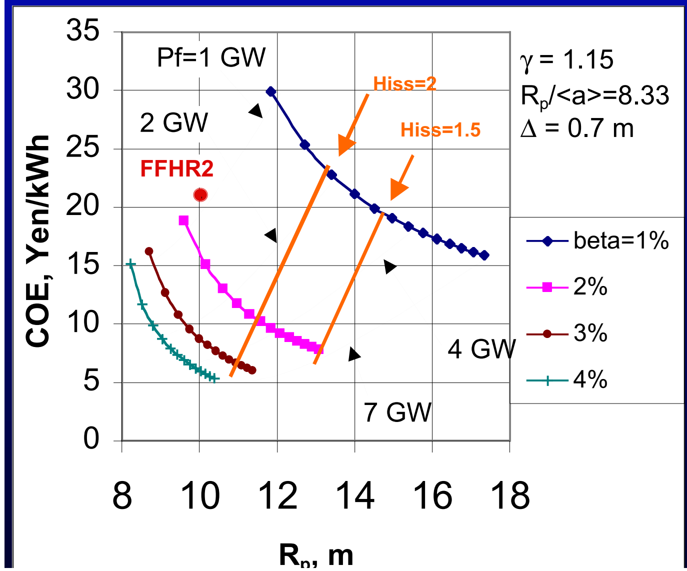
Cost Estimation
Using PEC code developed in NIFS.

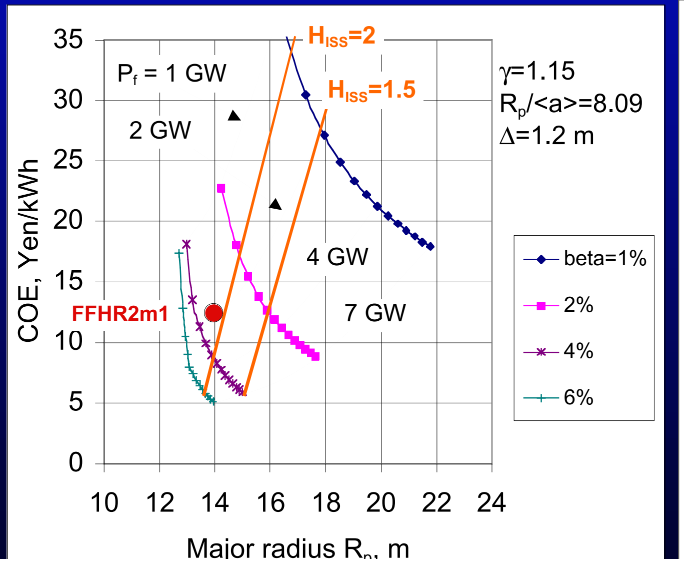
Calibrated with ARIES-AT, ARIES-SPPS, resulting in good agreement within 5 %.

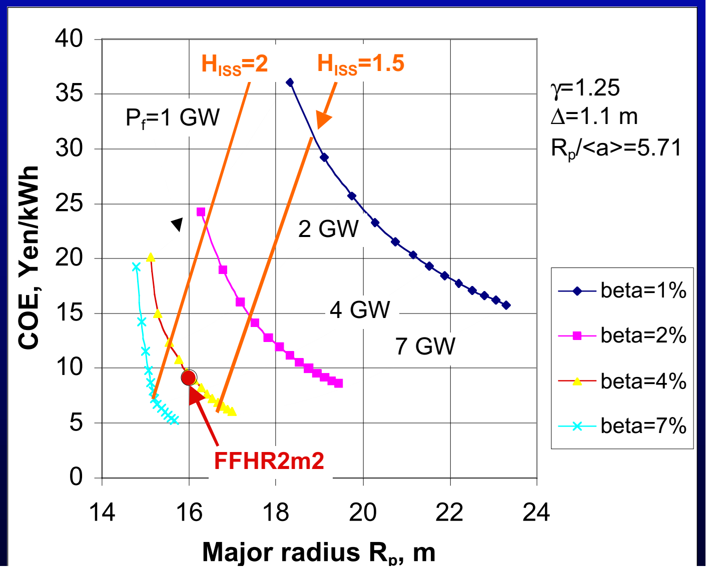
(T.J.Dolan,K.Yamazaki, A.Sagara, in press in Fusion Science & Tech.)

- **COE's for FFHR2, FFHR2m1 and FFHR2m2 decreases with increasing the reactor size,** because the fusion output increases in ~ R^2, while the weight of coil supporting structure increases in~ $R^{0.4}$ (not ~R^3).
- **When the blanket lifetime ~ 30y, the COE decreases ~20%** due to higher availability and lower cost for replacement.









Conclusions

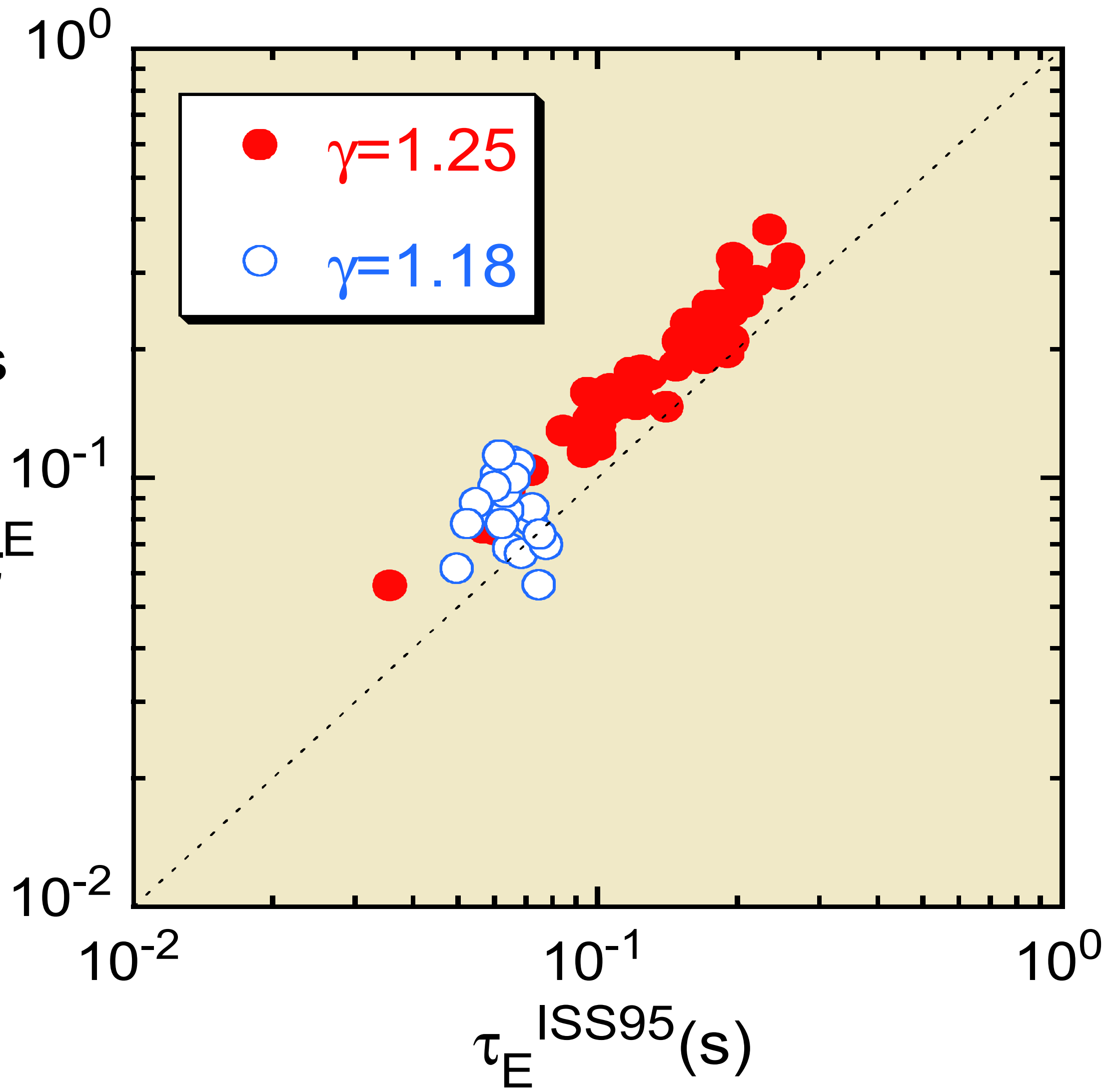
Design studies on FFHR have focused on new design approaches to solve the key engineering issues of blanket space limitation and replacement difficulty.

(1) The combination of improved support structure and long–life breeder blanket STB is quite successful.

(2) The "screw coaster" concept is advantageous in heliotron reactors to replace in-vessel components.

(3) The COE can be largely reduced by those improved designs.

(4) The key R&D issues to develop the STB concept are elucidated.



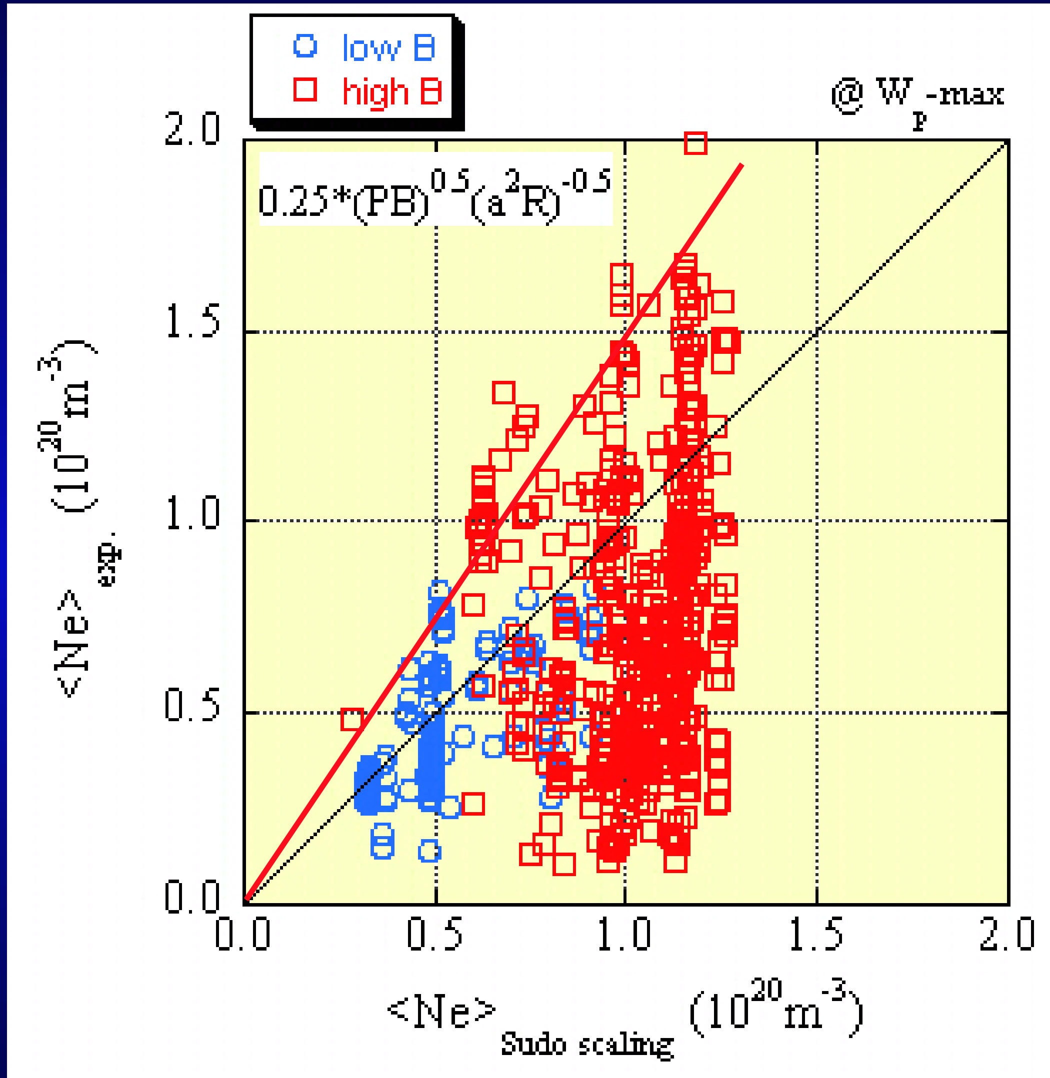
10^0
10^{-1}
10^{-2}
τ_E^{exp}(s)
γ=1.25
γ=1.18
10^{-2}
10^{-1}
10^0
τ_E^{ISS95}(s)

- Helical devices have radiative density limit which scales with square root of input power:

$$n_{H\text{-}E} \sim (PB/V)^{0.5} \qquad \text{(H-E Sudo)}$$

- LHD has a density limit which is **more than 1.4 times the Sudo limit**

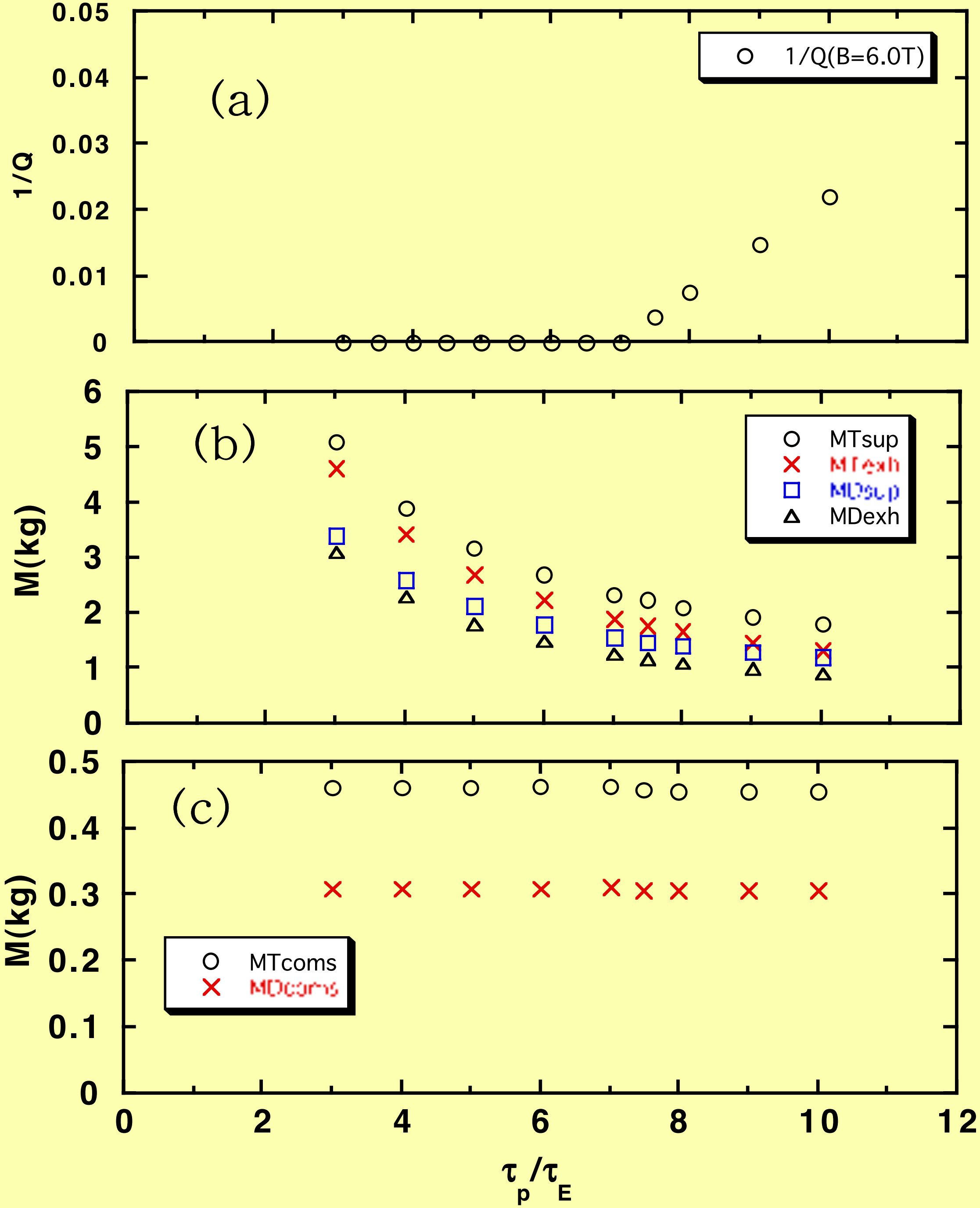
B.J. Peterson et al. NIFS
20th IAEA FEC EX6-2



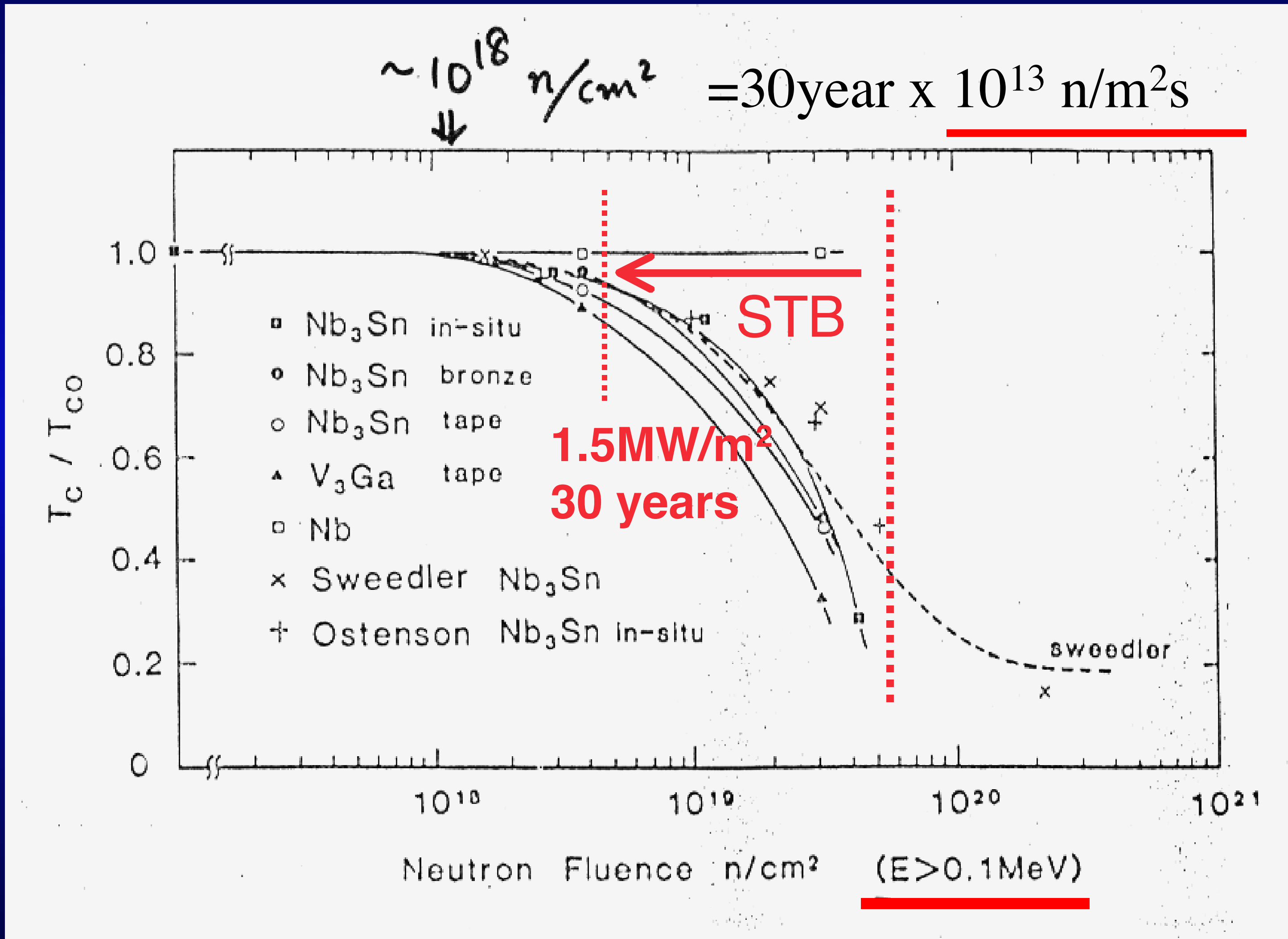
by K. Nishimura

$\tau_\alpha^*/\tau_E<7$

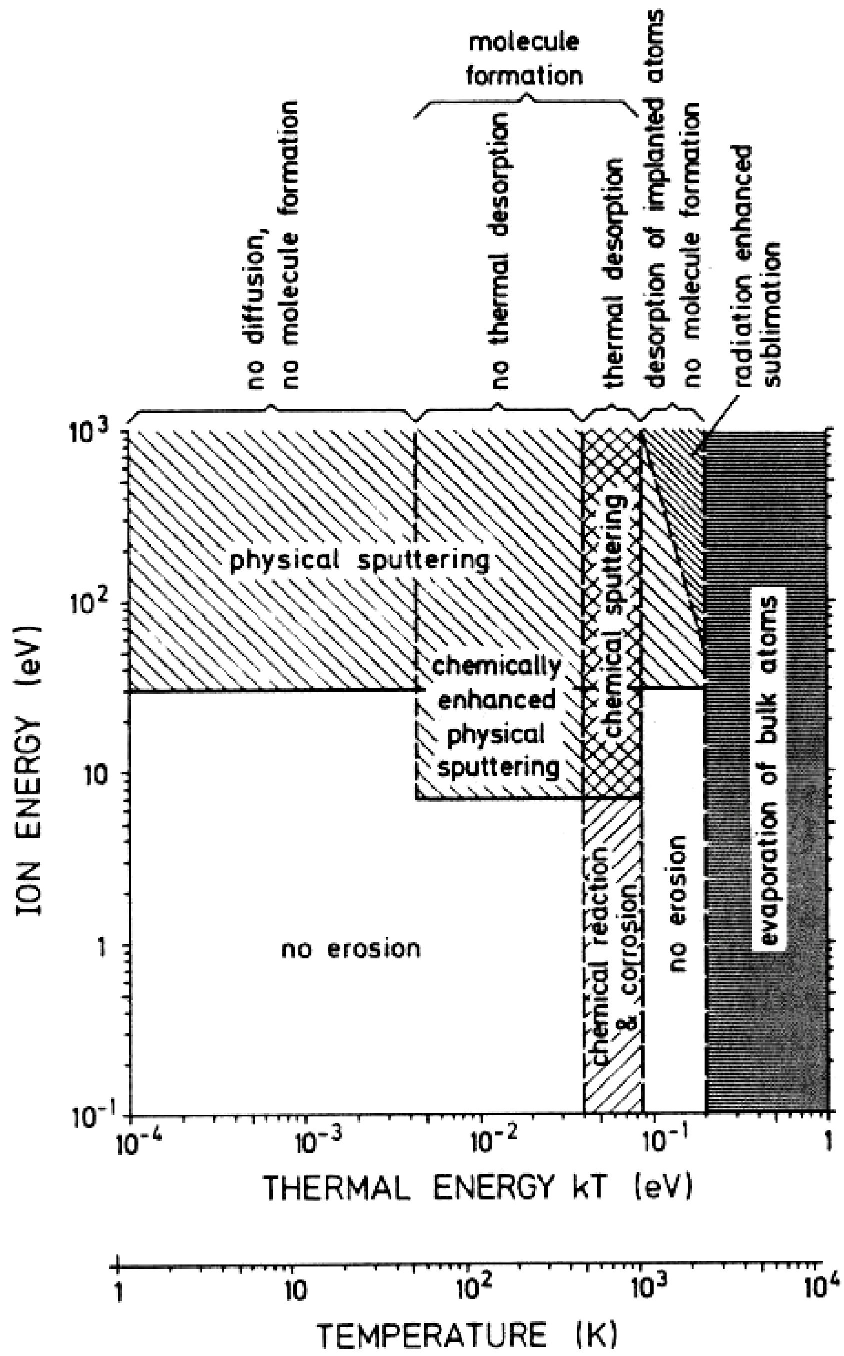
Tritium also pumped out



Dose effects of fast neutrons on SC magnets

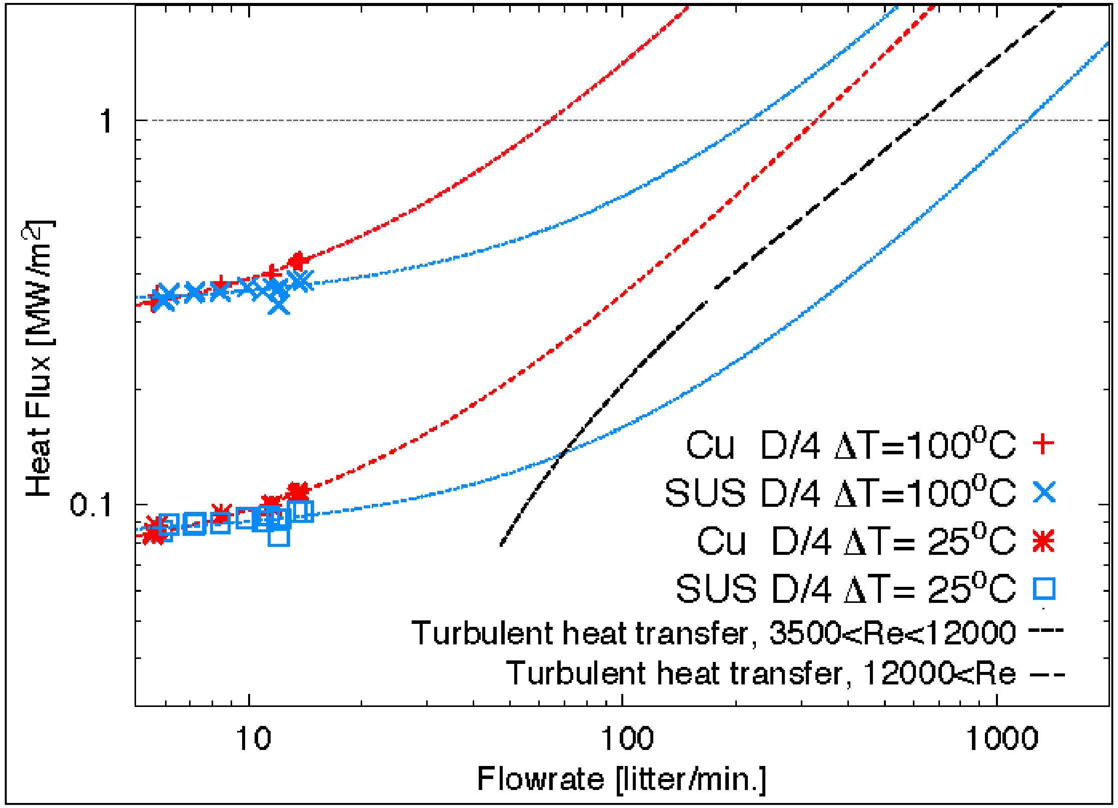


Kodama et al., JNM(1985) 819.

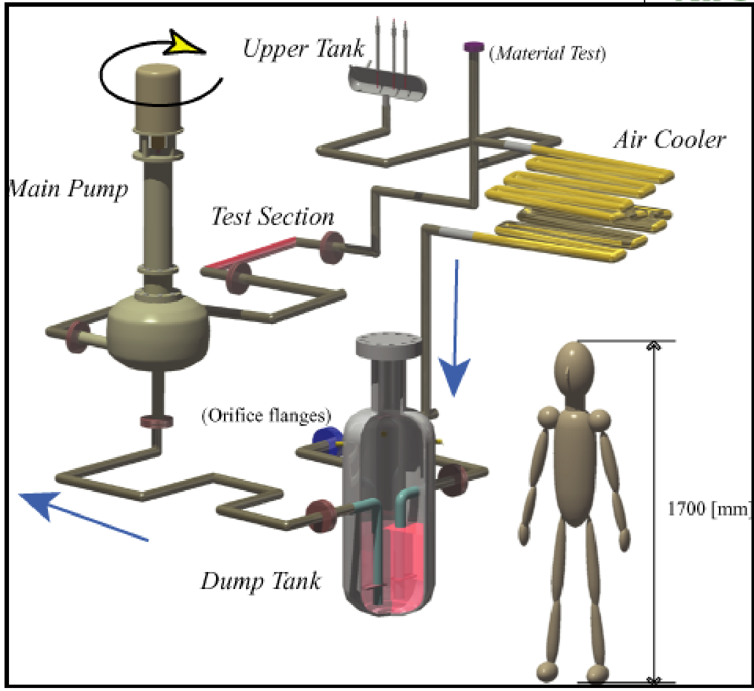


By J. Roth (1984)

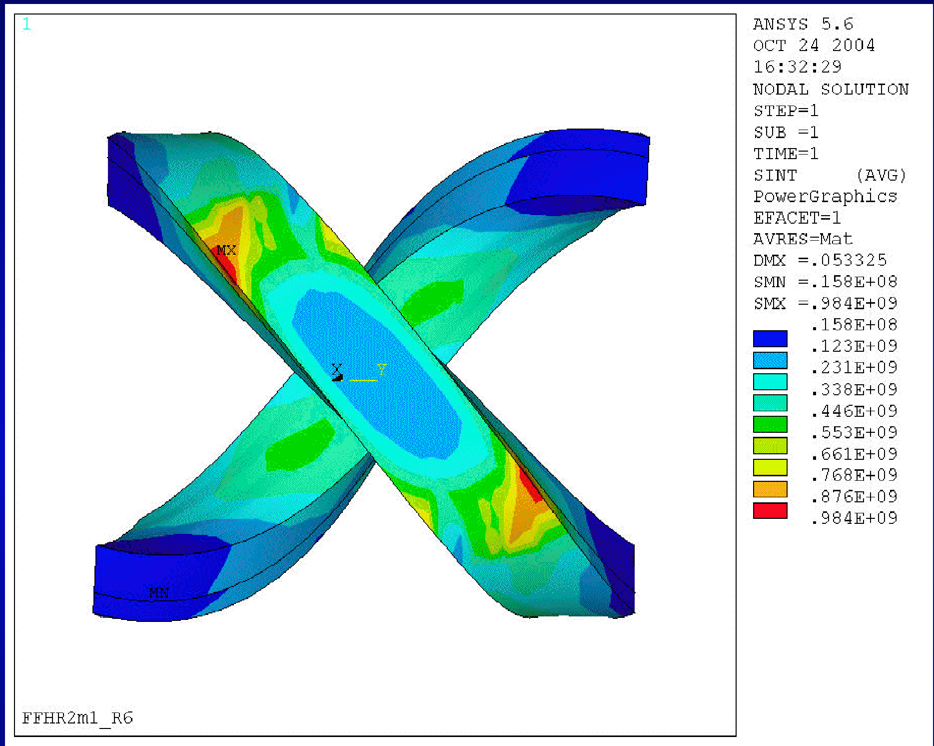
“TNT loop” (Tohoku-NIFS Thermofluid loop) has been operated using HTS (Heat Transfer Salt, T_m= 142°C)



TNT loop ~ 0.1m^3, < 600°C



- Results are converted into Flibe case at the same Pr=28.5 (Tin=200^{o}C for HTS and 536^{o}C for Flibe)
- Same performance as turbulent flow is obtained at one order lower flow rate.
- This is a big advantage for MHD effects and the pumping power.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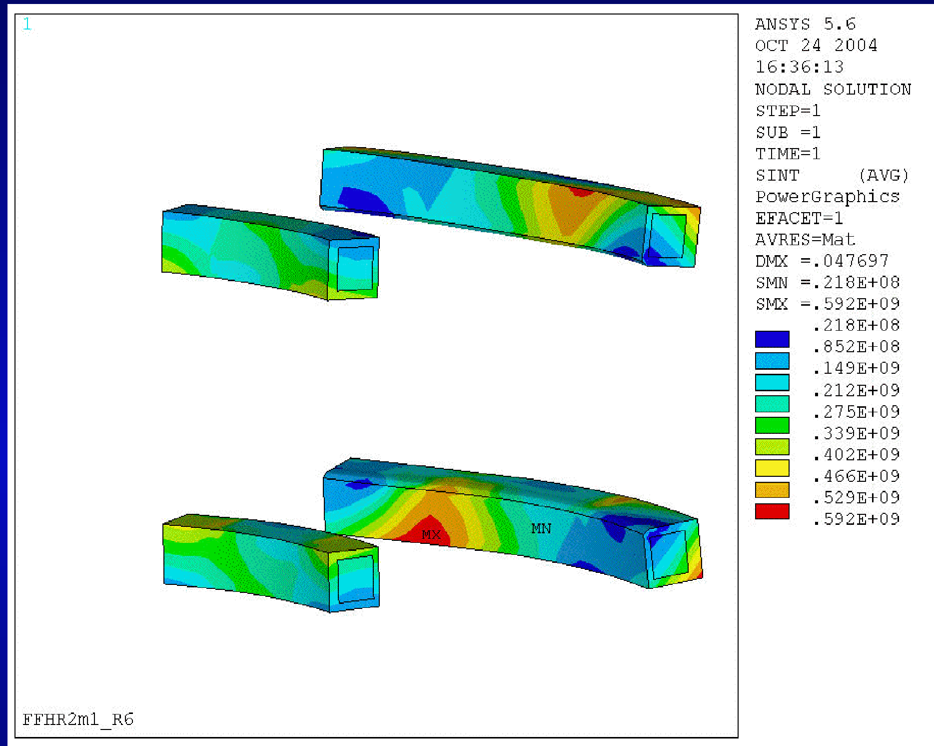
MX
MN
FFHR2m1_R6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